

Linearized elastodynamics

Barbora Benešová
in collaboration with
Malte Kampschulte and Martin Kružík

Modelling, partial differential
equations analysis and
computational mathematics
in material sciences

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FACULTY
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Charles University



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Harmonic oscillator

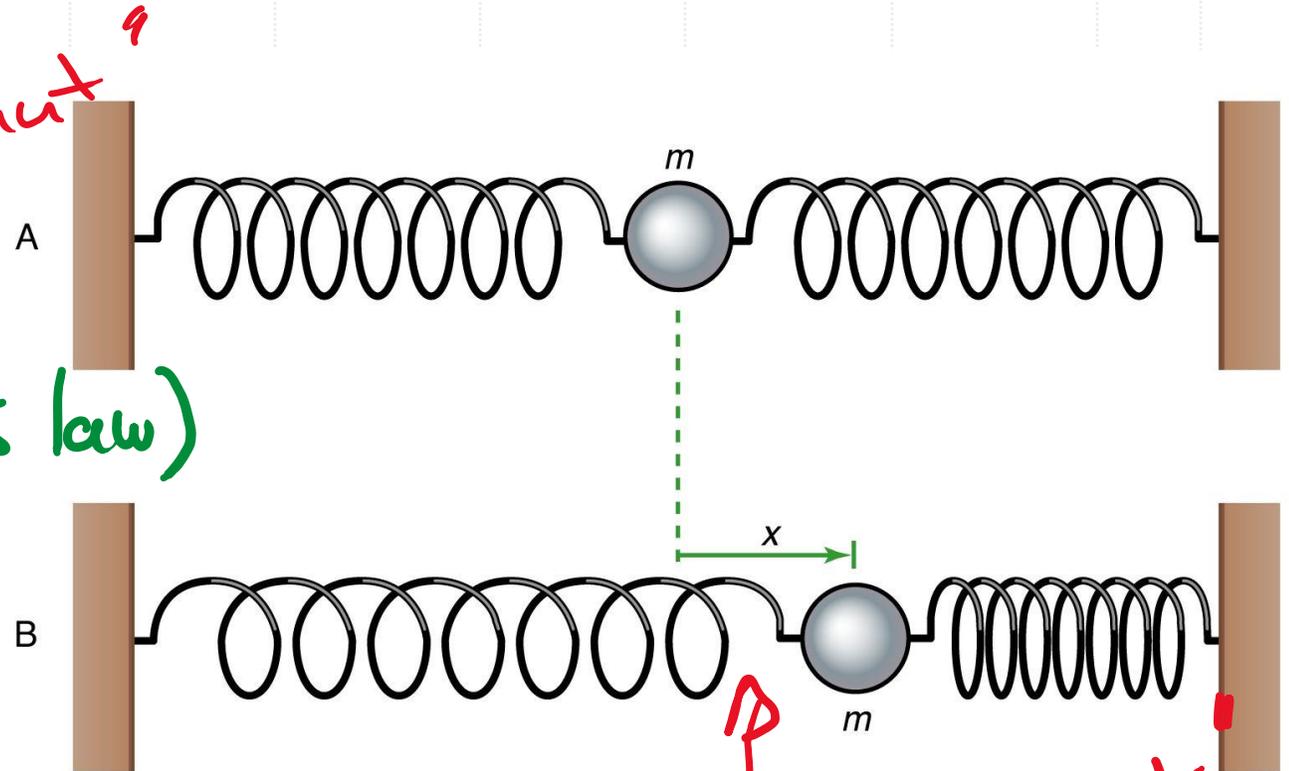
The force is a linear function of the displacement

$$f = -kx \quad (\text{Hooke's law})$$

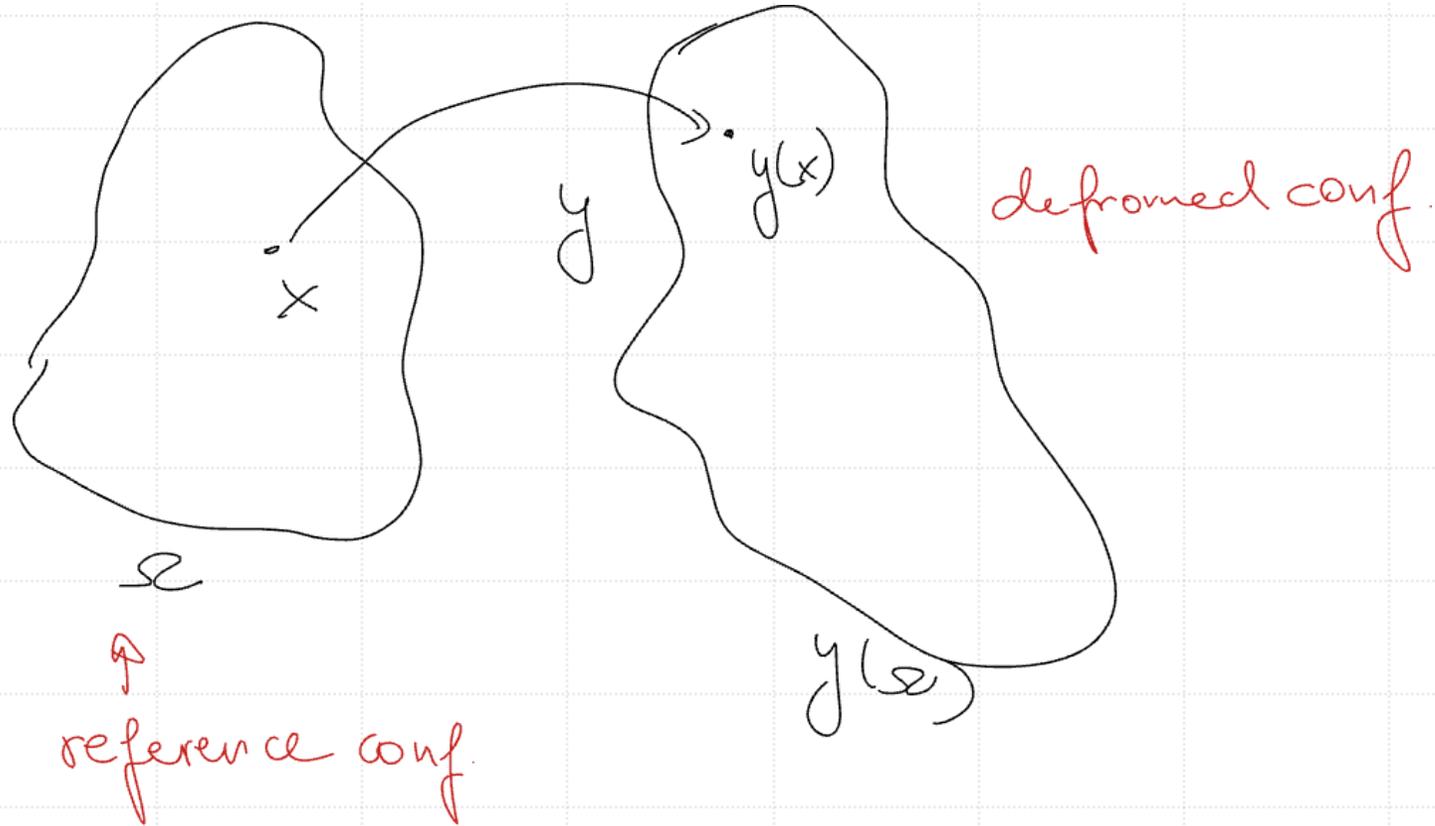
Therefore Newton's law can be written as

$$m\ddot{x} = -kx$$

mass



... in continuum mechanics



$$y(x) = x + \underbrace{v(x)}_{\text{displacement}}$$

... in continuum mechanics

The model in which the force is proportional to the strain is **linearized elasticity**

$$\rho \ddot{u} = f + \operatorname{div} \left(\mathbb{C} \left(\frac{\nabla_0 u + \nabla_0^T u}{2} \right) \right)$$

$\varepsilon \dots$ strain

where

$f \dots$ ext force

$\mathbb{C} \dots$ tensor of el. constants

The underlying energy:

$$w(\varepsilon) = \varepsilon \cdot (\mathbb{C} \varepsilon)$$

... in continuum mechanics

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**Only valid for
small strains....**

... large strain vs small strain

The model of linearized elasticity does not satisfy the physical principle of frame-indifference

and impossibility of infinite compression/orientation reversal

$$W(QF) = W(F)$$

with $Q \in SO(3)$

$$F = \nabla y$$

$$W(F) = +\infty \text{ if } \det F < 0$$

$$\Rightarrow W(F) \rightarrow \infty \text{ if } \det F \rightarrow 0^+$$

It only holds in the approximation when the displacement is very small so that

$$y(x) = x + \delta u(x)$$

$$F^T F = I + \delta(\nabla u + \nabla u^T) + \delta^2 \nabla u^T \nabla u$$

$$\sigma = \partial_F W(F) = \partial_F W(I) + \delta \underbrace{\partial_F^2 W(I)}_F \nabla u + \cancel{\sigma(\delta^2)}$$

Rigorous derivation - energies

Assumption

$$W(F) \geq \text{dist}^2(F, \text{SO}(3)), \quad W(I) = 0, \quad \int_{\Omega} W(I) = 0$$

$$\text{Set } I_{\delta}(v) = \frac{1}{\delta^2} \int_{\Omega} W(I + \delta Dv) dx$$

Theorem [Dal Maso, Negri, Percivale]

• If $I_{\delta}(v_{\delta}) \leq C \stackrel{\text{subs.}}{\Rightarrow} \exists v \in W^{1,2}$ s.t.
 $v_{\delta} \rightarrow v$ in $W^{1,2}$

• $I_{\delta} \xrightarrow{\Gamma} \frac{1}{2} \int_{\Omega} \varepsilon(\mathbb{C}) \varepsilon$ with $\varepsilon = \frac{(Dv + Dv^T)}{2}$

Rigorous derivation - energies

What this tells us is that "minimizers converge to minimizers"

$$u_\delta \in \arg \min_{\varphi \in W^{1,2}} I_\delta(\varphi) \quad u_\delta \rightarrow v \quad \text{so that}$$

$$v \in \arg \min_{\varphi} \int_{\Omega} \frac{1}{2} \varepsilon_j(\mathbb{F} \varepsilon_v)$$

It does not tell us

$$\text{if } u_\delta \text{ solve} \\ \mathcal{D}I_\delta(u_\delta) = 0$$

$$\text{then } u_\delta \rightarrow v \text{ \& } v \text{ solves} \\ \text{" } \operatorname{div} \left(\mathbb{F} \left(\frac{\partial v + \partial v^T}{2} \right) \right) = 0 \text{"}$$

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In fact, the Euler- Lagrange equation may be unrelated to the variational problem

[Dal Maso, Negri, Percivale, '02], [Ball, '85]

Rigorous derivation - energies

What this tells us is that "minimizers converge to minimizers"

$$u_s \in \arg \min_{v \in W^{1,2}} I_s(v) \quad u_s \rightarrow v \quad \text{so that}$$

$$v \in \arg \min_{\Omega} \int \frac{1}{2} \varepsilon_i (\mathbb{F} \varepsilon_v)$$

It does not tell us

if u_s solve

$$DI_s(u_s) = 0$$

then $u_s \rightarrow v$ & v solves

$$\text{" } \operatorname{div} \left(\mathbb{F} \left(\frac{\sigma_v + \sigma_v^T}{2} \right) \right) = 0 \text{"}$$

An even if it were, equi-coercivity is missing

[Dal Maso, Negri, Percivale, '02], [Ball, '85]

Fix I – obtaining the E.-L. eq.

Change the elastic energy a bit

$$\tilde{I}_\delta(u_\delta) = \frac{1}{\delta^2} \int_{\Omega} W(I + \delta D u_\delta) dx + \frac{1}{\delta^{p\alpha}} \int_{\Omega} |D^2 u_\delta|^p$$

with $p > 3, \alpha \in (0, 1)$

Theorem [Friedrich, Krůžík]

We have that $I_\delta(u_\delta) \xrightarrow{\Gamma} \int_{\Omega} \varepsilon(\varepsilon) dx$

In addition

$$\|D u_\delta - I\|_{L^\infty(\Omega)} \leq \delta^\alpha$$

↑
Notice the L^∞ !

[Healey, Krömer, 08],
[Friedrich, Krůžík, '17]
[Friesecke, James, Müller,
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Notice the L^∞ !

From now on, we will always use this modification

[Healey, Krömer, 08],
[Friedrich, Krůžík, '17]
[Friesecke, James, Müller, '02]

Fix II – equicoercivity

Still we face the problem of coercivity

for solutions $\{u_\delta\}_{\delta>0}$ of $DI_\delta(u_\delta) = 0$

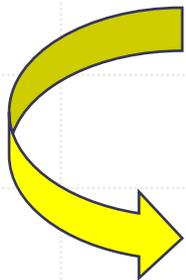
we don't know $J_\delta(u_\delta) \leq C$
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We actually want to consider the dynamic problem...

Dynamic model – variational approx.

Our problem can "informally" be expressed as

$$\rho \ddot{u}_g = \cancel{f_g} + \mathcal{D}I_g(u_g)$$

This can be approximated as

$$\rho \frac{\dot{u}(t) - \dot{u}(t-h)}{h} = \mathcal{D}I_g(u_g(t)) \quad \text{for } h > 0$$

"data = $f(t)$ "



discretize again for h fixed

Dynamic model – variational approx.

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This actually has only measure-valued solution, we should add dissipation

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Dynamic model – variational approx.

$$\int \frac{\dot{v}(t) - \dot{v}(t-h)}{h} = \mathcal{D}I_S(v_S(t)) \text{ for } h > 0$$

"data = $f(t)$ "

discretize again for h fixed, so
 $0 \leq j \leq 2J \dots \leq NJ = h$

$$\int \frac{v^k - v^{k-1}}{jh} = \mathcal{D}I_S(v_k) + f(jk)$$

Euler-Lagrange equation

$$\min_v \left[I_S(v) - \frac{f}{h} \int \left\| \frac{v - v^{k-1}}{j} \right\|^2 + \int f v \right]$$

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$$\min_u \left[I_S(u) - \frac{f}{h} \int \left\| \frac{u - u^{k-1}}{j} \right\|^2 + \int f u \right]$$

Discrete nonlinear problem

Dynamic model – weak solution

Theorem [B. Kampschulte, Schwarzacher]

The solutions to the disc. nonlinear problem converge upon taking $J \rightarrow 0$ & then $h \rightarrow 0$ to the weak sol. of

$$1) \int \ddot{u}_g = DI_g(u_g) \quad \& \text{ additionally}$$

$$2) \int_0^T \|\dot{u}_g(t)\| + I_g(u_g(t)) \leq \int_0^T \|\dot{u}_0\| + I_g(u_0)$$

Dynamic model – weak solution

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Technically, this is again cheating, because we should have included dissipation

Dynamic model – weak solution

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$$2) \int \|\dot{u}_g(t)\| + I_g(u_g(t)) \leq \int \|\dot{u}_0\| + I_g(u_0)$$

Notice that we now have the energies equibounded

[B., Kampschulte, Schwarzacher, '23], [Demoulini' 01]

Dynamic model – weak solution

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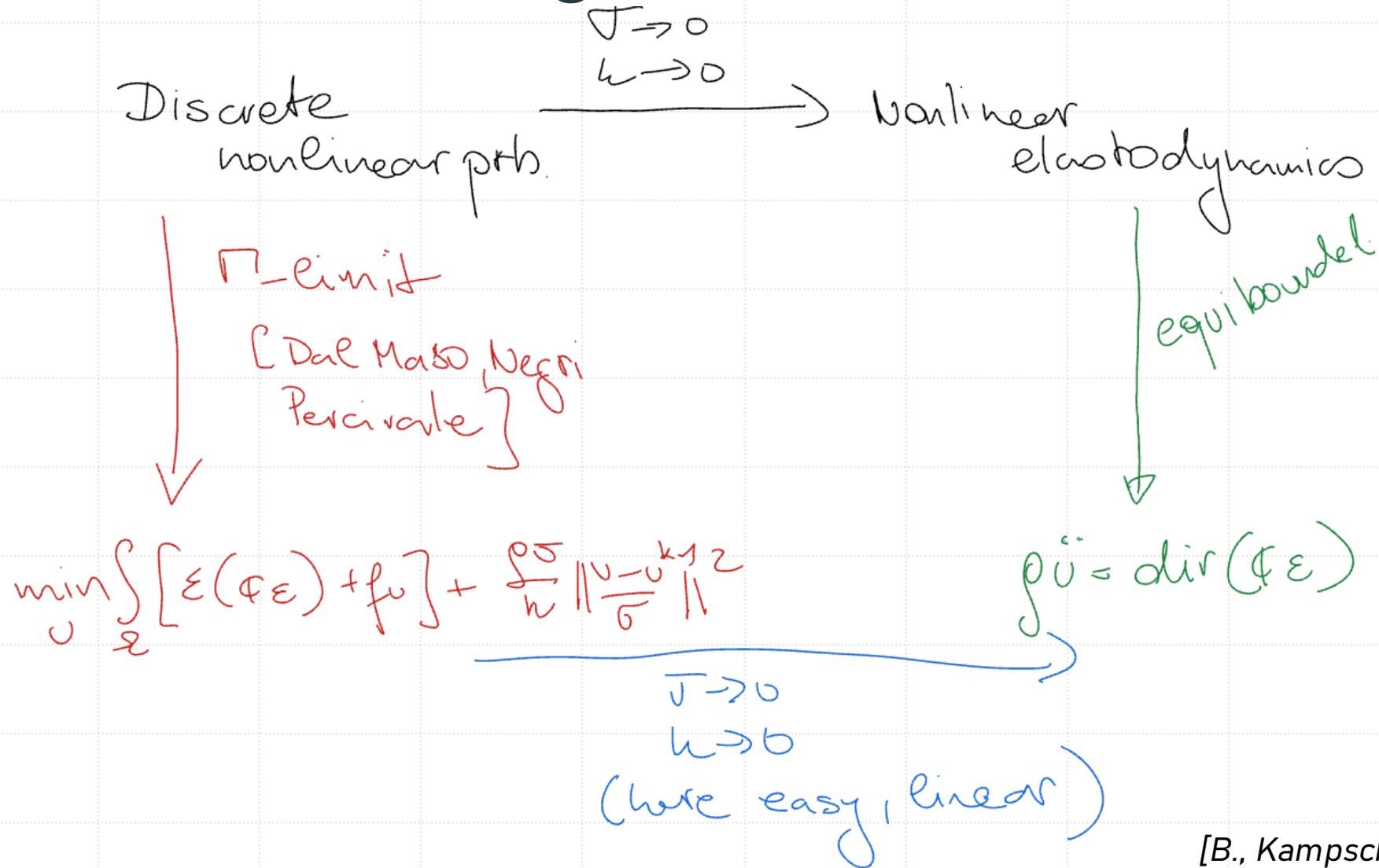
$$1) \quad \rho \ddot{u}_g = D I_g(u_g) \quad \& \text{ additionally}$$

$$2) \quad \frac{\rho}{2} \|\dot{u}_g(t)\| + I_g(u_g(t)) \leq \frac{\rho}{2} \|\dot{u}_0\| + I_g(u_0)$$

Weak solutions of (visco)elastodynamics can also be approached
by other methods, but...

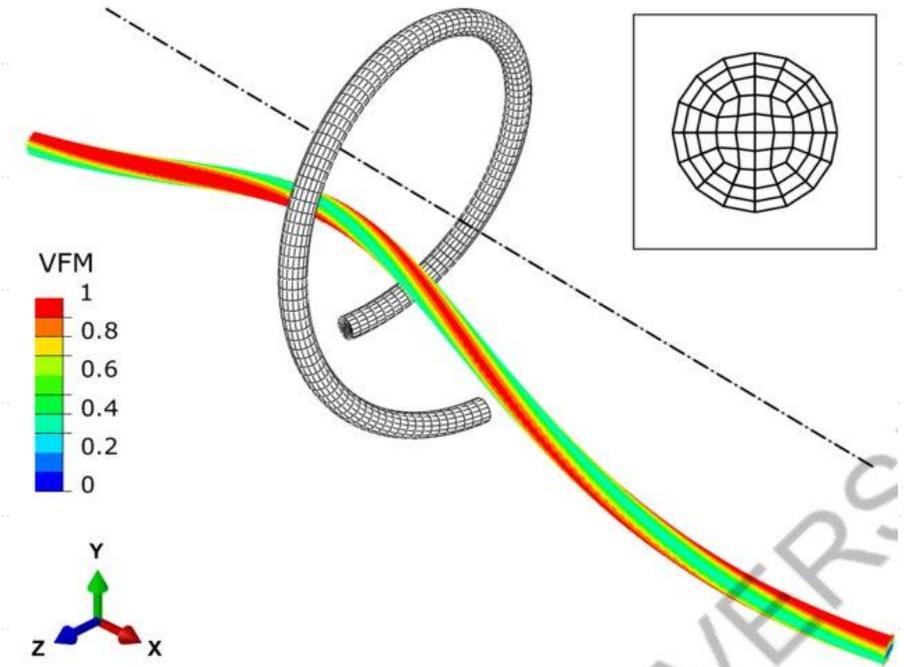
[B., Kampschulte, Schwarzacher,
'23], [Demoulini' 01]

Commutative diagram



Why study limits to the linearized setting?

- Probably the most used model in solid mechanics in engineering
- Can be coupled to inner variables, dissipation phenomena etc.
- Easy to verify, "only" 1 set of parameters
- The passage to the linearized setting in a sense justifies the non-linear setting



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Determination of All 21 Independent Elastic Coefficients of Generally Anisotropic Solids by Resonant Ultrasound Spectroscopy: Benchmark Examples

P. Sedlák · H. Seiner · J. Zídek · M. Janovská · M. Landa

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Abstract We present an experimental methodology for determination of all 21 elastic constants of materials with general (triclinic) anisotropy. This methodology is based on contactless resonant ultrasound spectroscopy complemented by pulse-echo measurements and enables full characterization of elastic anisotropy of such materials from measurements on a single small specimen of a parallelogram shape. The methodology is applied to two benchmark

reduces this number to 13 (monoclinic materials). The real triclinic symmetry class applies e.g. for certain types of minerals (talc [2] or albite [3]), superconducting iron-arsenides [4], or advanced perovskites [5, 6], etc. There have not been any successful attempts to determine full elastic tensors of such truly triclinic materials reported in the literature yet, although the well established ultrasonic methods (such as pulse-echo method [7], through-transmission



**Thank you for your
attention!**

Modelling, partial differential
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